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PROCESS FOR SUPPLYING PLASMA IONS

Takanobu Hashimoto

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# PROCESS FOR SUPPLYING PLASMA IONS

[Purazuma ion kyokyu hoho]

Inventor:

Takanobu Hashimoto

Applicant:

Fujikoahi Co., Ltd.

## Claims

- 1. A process for supplying plasma ions in hollow anode discharge tubes characterized in that a gas is introduced into the hollow tubes in the vacuum chamber and a dc anode electric potential is impressed thereto to allow anode discharge to occur in the hollow tubes, by which the introduced gas is energized to obtain cations from the hollow tubes.
  - 2. A process for supplying plasma ions in hollow anode

tubes being available in the forms of a hollow tube or a hollow polygonal pipe, with the tips processed into various shapes for realizing anode discharge in the hollow tubes.

- 3. A process for supplying plasma ions in hollow anode discharge tubes of Claim 1 wherein the anode electric potential impressed on the hollow tubes being 5 V to 30 kV, and made adjustable according to the kind, quantity, and pressure of the gas introduced as well as according to the length and cross section of the hollow tubes.
- 4. A process for supplying plasma ions in hollow anode discharge tubes of Claim 1 in which:
- (a) the hollow tubes being usable in a number of ways so as to individually impress an anode electric potential for realizing ionization by simultaneous introduction of several kinds of gases,
- (b) another hollow tube being placed inside the other tube keeping electric insulation and impressing the anode electric potential on the individual hollow tubes, and
- (c) it being usable in combination with various types of metal vapor generators.

# Detailed explanation of the invention

Industrial applications field

This invention relates to a process for producing a gasphase film normally using plasma (hereinafter called plasma CVD), and more particularly relates to a process for supplying plasma ions which can provide a remarkable increase in the ionization of the introduced gas and allow a plasma ion reaction to occur to a large extent, thus providing a compound film with the compositions unobtainable by conventional coating methods.

#### Prior art

In recent years, numerous methods of plasma CVD have been proposed, which are those utilizing a high-frequency capacity binding discharge, high-frequency induction binding discharge, microwave discharge, dc parallel plate discharge, their combined discharge, and combined use with a magnetron. On the other hand, another conventional method of ion plating is frequently used for film synthesis. However, these conventional methods are designated to attain the best possible ionization efficacy of evaporated substances in the gaseous form to increase the reaction, thus obtaining films which lack reactivity of the introduced gas and sealability with the treated substances of reactions (hereinafter called base plates), with their normal ionizations being 4% and at the most 40%.

Furthermore, when two or more different kinds of gases (including a compound gas and metal vapor) are simultaneously introduced to attain ionization, the difference in the linkage and combined state of each element not only makes it difficult to control the ionization, but frequently renders degradation of the introduced gas impossible. Therefore, it is extremely difficult to provide films with the desired compositions and structures.

In general, the properties of the formed films vary to a large extent according to the conditions such as vacuum degrees and process temperatures, possible contamination with foreign matter from an ion supplying source, residual impurities inside the vacuum chamber, and others, thus rendering the production of films with desired properties unattainable. Furthermore, for

example, with a thin film coating applied to a cutting tool and mold where extremely high coating sealability is requested, the lower ionization ratio and restricted processing pressure of conventional methods have made it extremely difficult to provide films with desired improvements.

On the other hand, an ion gun is available as a means for supplying ions at a relatively high ionization ratio, and the application has been tested for ion supply. However, the gun presently available requires various improvements before use in film production with plasma CVD or ion plating due to the following disadvantages: the complex structure, occurrence of high-voltage abnormal discharge, shorter service life of the thermal cathode PIG (Penning Ionization Gauge: thermal filament which generates electrons to produce plasma), the necessity of an electron supplying means, thermal filament contamination of the film material responsible for vacuum evaporation of the filament, and insufficient ion supply.

Problems to be solved by the invention

This invention was made through an evaluation of the above disadvantages and improvements of devices to solve the foregoing problems which are the insufficient ionization of introduced gases, poor increase in the ionization of each gas when two or more different gases (compound gas, metal vapor, etc.) are used in combination, the problem of controlling ionization, the problems of producing films with desired compositions, contamination of films resulting from the vacuum chamber and ion supplying sources, the sealability of coated films with the base plate of coated substances, etc.

Furthermore, this invention is to evaluate and solve the problems of conventional ion guns, such as complex structure, high-voltage-caused abnormal discharge, shorter service life, and insufficient ion supply.

In other words, this invention is to provide an ion supplying process which can easily attain extremely high ionization and large volume of ionization current at relatively low voltages from the gases containing the elements intended to be produced, thus leading to a vast improvement of the foregoing problems.

## Means to solve the problems

This invention is to provide a plasma-ion supplying process wherein gas is introduced into the hollow tubes placed in a discharge chamber (hereinafter called vacuum chamber) and the introduced gas is energized using the tubes to which a dc anode electric potential is impressed (hereinafter the hollow tubes to which a positive electric potential is impressed are called hollow anode discharge tubes) to obtain cations from the hollow anode discharge tube), thus solving the foregoing problems.

The hollow anode discharge tubes can take any shape, including cylindrical or polygonal ones, as long as they are hollow, with the shapes made adjustable according to the vacuum degree of the vacuum chamber containing an introduced gas and the devices and machines in and around the chamber. Ionization is to be adjusted by controlling the anode electric potential impressed on the hollow tubes, with the applicable anode electric potential being 5 V to 30 kV. Furthermore, when the simultaneous introduction of gases (plural) is made to attain ionization, the above problems can be settled using a number of hollow anode

discharge tubes to which an anode electric potential can be individually impressed, or using the anode discharging tube structured so as to have another hollow tube inside one hollow tube, with electric insulation maintained, or by the combined use with various types of metal vapor generators. Furthermore, by this invention there is a structure simplified to the greatest possible extent provided to prevent the abnormal discharge and to prolong the service life of ion supplying devices.

#### . Functions

As exemplified by the device given in Figure 1, this invention is to introduce gas into hollow tube (1) and to impress a dc anode electric potential thereto causing hollow anode discharge, thus energizing the introduced gas to produce cations, with the structure made so as to easily produce discharge by impressing the proper dc anode electric potential to hollow tube (1), attracting all the existing electrons to allow the discharge to start.

In this instance, the discharge occurs and continues to occur in vacuum chamber (7) connected to the grounded electric potential, or between base plate (6) or base support (5) to which a grounded electric potential, cathode electric potential, or anode electric potential lower than the dc anode electric potential impressed to the hollow anode discharge tube is impressed.

When discharge starts inside said hollow anode discharge tubes, there is a collision of electrons accelerated toward the hollow anodes with the introduced gas and the gas is ionized with emitting electrons, then the emitted electrons cause recollision with another introduced gas, thus repeating the

collision/ionization and continuously increasing the number of electrons and ions to provide an extreme potential discharge phenomenon. A proper modification of the hollow tube shapes and control of the anode electric potential to be impressed can provide every introduced gas with collision/ionization, thus attaining ionization up to 80%, which may vary with the kinds of gases introduced.

In this instance, whereas electrons are attracted to the hollow anode discharge tubes and disappear, the cations remain and are subsequently provided as a large cation flow to the negative plates (such as vacuum chamber (7) and base plate (6), etc.). Ionized atoms are attracted to the negatively impressed base plate (6) and an adequate control of the voltage will enable ion etching and ion infusion film synthesis, thus attaining extremely high sealability.

We have found that various gases can be treated in a device so structured as claimed in this invention and have realized this invention. We have not theoretically elucidated the mechanism of the hollow tube anode discharge, but have found an adequate modification of the hollow anode discharge tube shapes and proper control of the vacuum degree upon discharge and ionization, as well as anode electric potential providing a simply structured means to realize a large amount of ion supply and extremely high ionization. Besides, adequate conditions of hollow tube shapes, vacuum degrees at the discharge, and ionization, as well as anode electric potential will be determined by the dimensions and shape of the vacuum chamber, kinds of introduced gases, and the compositions of the films to be produced. Special attention should be given to the dc anode electric potential to be impressed on the hollow tubes, with a potential range of +5 V to

+30 kV. Ionized energy of normally existing elements are said to be 5 ev to 25 ev.

Therefore, the voltage of 5 to 30 V will cause ionization; when the introduced gas is a compound it will cause less ionization, in most cases requiring a voltage of more than 25 V. Furthermore, an improved ionization will necessitate an increase in the impressed voltage which then raises the frequency of problems such as abnormal discharge, heating resulting from electron collision in the hollow anode discharge tubes, and other abnormalities of attrition. Therefore, the maximum voltage is determined to be 30 kV.

When two or more different ions are supplied by the simultaneous use of two or more different gases to provide a compound film or alloy film, in order to realize an increased ionization for each introduced gas, as shown in Figure 5, two or more of the hollow anode discharge tubes are placed in parallel, or as shown in Figures 6 and 7, the hollow tubes are structured to have another hollow tube inside a given hollow tube, i.e., a multiplated and multilayered structure, thus impressing each anode electric potential with individual electric sources, and making it possible to control degradation, energizing, and ionization by adjusting the discharge intensity for each introduced gas. In general, a metallic ion is the lowest in ionization potential, followed by an active gas, then an inert gas; when a compound gas is used, it requires an even larger ionization energy due to the necessity of decomposing each linkage and energizing gas for ionization. Thus, as mentioned before, the use of multiplated and multilayered hollow anode discharge tubes realizes the ion supply according to need and provides the films with the desired properties.

On the other hand, an irradiation of Ar ion and others supplied through hollow anode discharge tubes to base plate (6) will cause collision of inert ions on the base plate to clear the base surfaces, thus increasing the sealability of the formed film with the base plate, which an be easily obtained by selecting the gases to be used and adjusting the impressed anode electric potentials in the hollow anode discharge tubes.

Furthermore, provision of base heater (8) will be of help in heating and removing impurities, for example, halogens such as TiCl<sub>4</sub> in the introduced gas attached on the base plate surfaces, or further in increasing hollow anode discharge utilizing heated electrons from the heater. Insulator (13) provides base heater (8) with electric power from heater power source (3). The foregoing process is to provide the desired film compositions, improving film properties, and drastically improved sealability of the synthesized film with base plate (6) by supplying highly activated ions.

Additionally, this invention has provided a process for ion supply, the structure of which is simplified to the best possible degree unlike the conventionally used ion gun, to have the least frequency of abnormalities, which is almost free of abnormally high temperatures and attrition of hollow anode tubes and provided with an extremely long service life because of the singular collision of electrons in the hollow anode, and which is free from the contamination of film materials resulting from fused evaporation of tube materials.

#### Embodiments

The present invention will hereinafter be described in practical terms, with reference to the attached figures.

However, the invention is not limited thereto. The same symbols given in the figures mean the same or similar materials.

Figure 1 shows an example where hollow anode discharge tube (1) is singularly used to realize the production and radiation of the desired ion using one of the introduced gases selected from inert gases such as Ar, Ne, etc., metallic gases such as SiH4, TiCl4, etc., or organic metal compound gases such as  $Ti(N(CH_3)_2)_4$ , and further to realize ion cleaning or ion etching with an inert gas ion, or to realize the production of a metallic film and the synthesis of compound films. Hollow anode discharge tube (1) is made with conductive hollow tubes of such materials as Ta, Mo, W, or stainless steel, with the above-mentioned gas being supplied to hollow tube (1) via flowmeter (15) and gas flow regulating valve (14) from gas supplying source (16). On the other hand, the hollow anode discharge tube (1) is connected to the anode electric potential of the power transformer (2), keeping electrical insulation with the vacuum chamber or gassupplying mechanism via insulator (11).

Vacuum chamber (7) is connected to the outside evacuator with evacuation hole (10) for evacuation, electrically grounded in most cases. In this instance, the vacuum degree used is from several + Torr to 10<sup>-3</sup> Torr. An introduction of the foregoing gases into the hollow anode discharge tube structured as mentioned before to impress an anode electric potential will enable remarkable collision and ionization of electrons with the introduced gas, irradiating and supplying the generated ions to vacuum chamber (7), especially to base support (5) or base plate (6) negatively impressed at power transformer (4) shown in the figure, power transformer (4) and vacuum chamber (7) are insulated with insulator (12). When the introduced gas is an inert gas such as Ar, base plate (6) is subjected

the gas is  $SiH_4$ , base plate (6) forms a Si film hereon, with the Si ion implanted thereto in some cases. Furthermore, when the gas is a compound such as  $Ti(N(CH_3)_2)_4$ , the compound film such as Ti(CN) is allowed to form on base plate (6).

Thus, selecting an introduced gas suitable for the applications and adjusting the anode electric potential have provided a process capable of ion etching, ion infusion, and film synthesis.

Normally, the dc electric field causes the introduced gas to discharge, with the voltage capable of degrading compounds and energizing ionization being several + Torr to  $10^{-3}$  Torr as mentioned before. However, when improvements are required to prevent contamination of base plate (6) resulting from the absorbed gas on the inner surface of vacuum chamber (7) or to increase the mean free path of the ions, and in some cases the vacuum degree in vacuum chamber (7) should be raised to  $10^{-4}$  to 10<sup>-9</sup> Torr. Alternatively, in this instance, the pressure in the hollow tube can be kept at several Torr to  $10^{-2}$  Torr to maintain stable discharge conditions, with hollow tube (1) tapered as shown in Figure 2. On the contrary, when stable discharge is desired to continue at several + Torr, stable discharge can be obtained by providing the structure so as to produce the least possible pressure difference between the inside of hollow tube (1) and vacuum chamber (7), with the tip of the tube opened, as shown in Figure 3.

Furthermore, in Figure 1, normal discharge will stably continue between hollow anode discharge tube (1) and base plate (6) negatively impressed thereby, but intermittent abnormal discharge may occur between tube (1) and vacuum chamber (7) when the positive electric potential impressed on the tube is several + kV to several tens of kV. In particular, when prolonged

discharge is required with the electric potential in the tube kept raised, an occurrence of abnormal discharge is to be prevented by applying insulating material (9) of  $Al_2O_3$  by injection or other means to provide the tube surfaces with coating. The insulating material to be coated, for example,  $Al_2O_3$ , the thickness of which can vary to a large extent with the insulation degree based on the pore ratio and compositions of  $Al_2O_3$ , will normally suffice at 50  $\mu m$  to 3 mm for a large insulation degree, and will peel off the hollow tubes due to the high possibility of cracks resulting from the temperature difference between the pre- and postdischarge for a thickness exceeding these ranges.

Figure 5 shows a practical process for attaining simultaneous supply of a number of ions by the combined use of two or more different gases. Hollow anode discharge tubes (1-1) (1-2) are individually connected to the anode sides of powder transformer (2-1) (2-2), and the respective tubes provides gas via gas regulating valves (14-1) (14-2) from the gas supplying source. Electric insulation, vacuum degree on discharge, shapes of the hollow tubes for realizing discharge, and the impressed electric potential are all within the preceding ranges. Thus, an impression of anode voltage suitable for the chemical linkages of a number of gases using a number of hollow tubes has realized the gas supply for the intended purposes, and has attained stoichiometrically produced films, compound films, or alloy films with further desirable properties.

Additionally, Figures 6 and 7 show processes for producing compound films with desired compositions by arranging double- or triple-structured tubes, or two or three pieces of the tubes in a hollow anode discharge tube even for the difficulty in mixing the introduced gas. In this instance, also, the impressed anode

electric potential, shapes of the hollow tubes, and vacuum degree on discharge are all within the foregoing ranges.

# Application Example 1

A production of TiCN film was carried out by the use of  $Ti(N(CH_3)_2)_4$  as an introduced gas in the device shown in Figure 1 under the following conditions:

Hollow anode voltage	+1500 V
Pressure in the vacuum chamber	$1 \times 10^{-1} \text{ Torr}$
Dimensions of hollow anode discharge tube	$\phi$ 25 mm x <u>1</u> 100 mm
Electric current in the tube	4.5 A to 4.2 A
Base plate voltage	-500 V
Base plate heater	20 V 100 A to OVOA
buse process	(SUS band heater)
Estimated temperature of the base plate	300-400°C
Base plate material	HSS chips (type
	similar to SNGN <sub>432</sub> )

The thus-obtained film is a silver-gray-colored TiCN film with a composition resembling that of TiC, HV 2000-2200, and determined to be  $\text{TiC}_{0.7}\text{N}_{0.3}$  from X-ray diffraction.

The continuous machining test of  $S_{45}C$  (HB<sub>180-200</sub>) processed into HSS chips (SNGN<sub>432</sub>) has revealed that the processed substance has about a 5 times longer life than unprocessed.

# Application Example 2

TiN film production was carried out using  $\text{TiCl}_4$  as an introduced gas and  $N_2$  as a reaction gas in hollow anode discharge

tubes (1-1, 1-2) of the device shown in Figure 5 under the following conditions:

Hollow anode discharge tube
.Hollow anode voltage
Dimensions of the hollow anode tube

Introduced gas
Electric current of the tube
Pressure of the vacuum chamber
Base plate voltage
Base plate heater

Estimated base plate temperature Base plate material

+1300 V +1500 V  $\phi$  20 mm x  $\frac{1}{2}$  100 mm  $\phi$  25 mm x  $\frac{1}{2}$  100 mm TiCl<sub>4</sub> H<sub>2</sub> N<sub>2</sub> 2.5 A to 2.8 A 3.8 A 1 x 10<sup>-2</sup> Torr

1-2

1-1

-800 V 20 V 100 to 10 V 5.5 A (SUS band heater) 400-500°C

HSS chips (type similar to SNGN<sub>432</sub>)

The obtained film was gold-colored TiN with the composition of HV $_{1800}$  to 2000, containing a trace of 0.5% Cl. The film was processed into HSS chips to produce  $S_{45}C$  (HB $_{180-200}$ ) which was then subjected to a continuous machining test. The test revealed that the processed structure has about 4 times longer machining life than unprocessed. A comparison with normal plasma CVD showed the thus-processed film was excellent in sealability, free of peeling, and was provided with larger ion-supplying effects resulting from the hollow anode discharge.

Effects of the invention

The plasma-ion supplying device based on this invention has

- (a) supply of highly reactive plasma ions with high ionization and extremely high ion density;
- (b) supply of ions at the highest controlled ionization level by altering the dimensions of the hollow tubes and adjusting the quantity of introduced gas and the impressed anode voltage depending on the energy needed to decompose the gases and to cause energized ionization, when two or more different gases were used together;
- (c) adjustment of the film compositions formed by the effect mentioned in (b) to the most desirable compound;
- (d) prevention of film contamination responsible for vacuum evaporation of heat filament elements as with the thermal cathode PIG ion gun, easy supply of a large magnitude of ion electric current, simplified structure almost or completely free from the occurrence of abnormalities;
- (e) the hollow anode discharge tube receives only a small magnitude of electron collision, being free of damage and provided with a resultant prolonged service life of the tubes;
- (f) any element in gaseous form being convertible into ions, with high-density ions being suppliable;
- (g) the introduction of inert gases such as He, Ne, and Ar into the hollow anode discharge tubes and irradiation of ionized gas on the base plate can provide the base plate surface with ion etching and ion cleaning, further providing continuous synthesis of compound films only by changing the reaction gas, and attaining extremely high sealability of the film with the base plate.

## Brief explanation of the figures

Figure 1 shows a device for supplying plasma ions in this invention; Figure 2, 3, and 4 show structures of the hollow tubes; and Figures 5, 6, and 7 show other devices of this invention.

1...hollow tube (1-1, 1-2, 1-3 all similarly arranged);
2,4...power transformers (2-1, 2-2, 2-3 all similarly arranged);
5...base support; 6...base plate; 7...discharge chamber (vacuum chamber); 8...substrate heater; 10...evacuation hole;
11,12,13...insulator; 14...gas control valve (14-1, 14-2, 14-3 all similarly arranged).

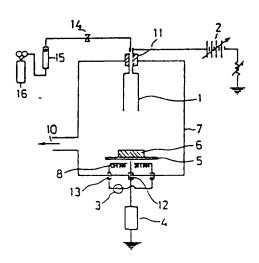


Figure 1

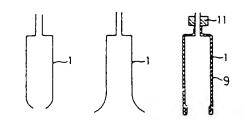


Figure 2 Figure 3 Figure 4

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プラズマイオン供給方法 公発明の名称

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砂発 明 者 本 孝 信 富山市石金20番地 株式会社不二越内

株式会社不二越 宣山市石金20番地 卯出 願 人

弁理士 河内 潤二 の代 理 人

発明の名称

ブラズマイオン供給方法

- 特許請求の範囲
- (1) 放電室内に設置された中空管内にガス体を導 入し、その中空管に直旋陽極電位を印加し中空 陽極放電を生ぜしめることにより導入ガス体を 励起し、中空管より降イオンとして引き出すこ とができることを特徴とする中空陽極放電形プ ラメマイオン供給方法
- (2) 前記中空管の形状は中空円筒あるいは中空多 角形状パイプをなし、中空陽極放電を可能なら しめるため、先端形状を各種形状に加工したも のを用いる特許請求の範囲第1項記載の中空陽 極放電形プラズマイオン供給方法

1. 発明の詳細な説明 (産業上の利用分野)

本発明は、通常プラズマを用いる薄膜の気相合 成(以後プラズマC ▼ D という)方法に係り等に 導入ガス体のイオン化効率を着しく大ならしめ、 プラズマイオン 反応を積極的に可能にし、従来の コーティング方法では調整不可能な化合物組成模

(4) 複数のガス体を同時に導入し、イオン化を計 ることを目的とする場合、各々陽極電位を印加

できる前配中空管を複数備並用したり、1つの

中空管内に別の中空管を電気的絶縁を計りつつ

各々の中空管に降極電位を印加しながら配置し

たり各種金属蒸気発生装置等と並置して使用す

ることの可能な特許請求の範囲第1項記載の中

空陽極放電形プラズマイオン供給方法

は中空管の長さ、断面機に応じて調整できなり のとした特許請求の範囲第1項記載の中空陽極 放電形プラズマイオン供給方法

近年プラメマCVDの手法として高周波容量結 合放電型、高周波誘導路合放電型、マイクロ波放

## 特開昭61-143579 (2)

電型直次平行平板放電型及びそれらの組み合せ型、マグネトロン併用型等多数の方法が提案されている。 では、大きなないないでは、大きなないないでのでは、大きなないが、大きなないが、大きなないが、大きなないが、大きなないが、でのでは、ないの反応性が不足になって、との告性が不足している。

しかも二つ以上の異種ガス(化合物ガス、金属 蒸気をも含む)を同時に導入しイオン化を計る場合各元素毎に結合、化合の様子が異なるためイオ ン化。関節が困難であるばかりでなく、導入ガス体の分解すら不可能を場合が多い。 従って生成され る模材質に期待する組成・構造を持たせることが 非常に困難である。

一般に生成された模特性は、処理真空変、処理 進度、イオン供給原からの不規物混入、真空チャ ンパー内機留不純物元素の混入等処理条件によっ

本発明は上記問題点を検討し装置改良を積み重ねて発明に致ったもので、前配導入ガス体のイオン化率不足に関する問題、二つ以上の異種ガス(化合物ガス、金属蒸気等)のそれぞれのイオン化本向上と、イオン化の調節に関する問題製質組成コントロールに関する問題、真空窒、イオン供の素から発生する模方染に関する問題、被覆膜の基板との密着性に関する問題等の解決を計るととを目的とする。

さらに従来イオン庄入に使用されているイオン 銃の理維構造や高電圧に基づく異常現象の発生、 寿命、イオン供給量の不足等種々の問題点を検討 し解決を計る。

・ 即ち本発明は合成しようとする目的元素を含む → ・体を主義が近し業所で、第二(本の)。

供服力供支援供心 分配問題点を大幅化改善》 能化した。

(問題を解決するための手段)

7 7 - 2

本発明は放進室(以下真空チャンパーという)

て押しく変化するため、要求される種々の集合収 に対応できていない。さらに、例えば切削工具、 全型等への薄膜コーティングの如く、極めて高い 被覆裏密着性を要求される場合、従来方式による コーティングではイオン化率が低く、処理圧力上 の制限等により任意に改善することが非常に困難 である。

内に設置された中空管内にガス体を導入し、その中空管に直促陽極電位を印加した中空管(以後正電位印加した中空管を中空陽極放電管という)を用い、導入ガスを励起し中空陽極放電管より陽イオンとして引き出すことができるブラズマイオン供給方法を提供し前記問題点の解決を計るものである。

A 4 19 18 19 18

選挙用したが、 ・中で管内に別の中で言とも 気的絶験を計りつつ配置した陽像放電管構造を出いたり、各種金属蒸気発生配置と並用して使用することも可能にして前配権 4 の問題点解決を計る。

#### 特開昭61-143579 (3)

また出来る限り構造簡素化を計り異常現象の発生 を防止し、イオン供給装置の海命向上を可能にする。

#### (作用)

放電が開始されると、前配中空陽極放電管の内部では中空陽極に向って加速された電子と導入ガス体が衝突し、導入ガスは電子を放出してイオン

道正化するとで、比較的個素な構造でイオン化字が著して大きく大量のイオン供給が可能なる方法を生み出したものである。尚、中空管形状、中空度である。尚を生みなどである。 はない はない である。 しかし 特に 留意する である。 しかし 特に 留意 すで の で の で る 直 で で を で か ら 2 5 €♥ と こ で で か ら 2 5 €♥ と こ で か ら 2 5 €♥

イオン化化要する電圧は従って5~30 V で可能となるが導入ガス体が特に化合物である場合イオン化の割合いが小さくなり通常25 V 以上が好ましい。さらにイオン化率向上のため印加電圧を

であ、消耗等具常発生の頻度が高まる。ほうて実 用上上限 3 0 KV に限定される。

さらに二つ以上の異種ガス体を同時に用い、二

. - .

化し、放出された電子は再び別の導入ガス体と衝突し次々に電子、イオン数を増すような衝突電離をくりかえし、著しく大きな放電現象を誘発するようになる。前配中空管(1)の形状、印加する陽低電位等を通切に調整することにより、導入ガス体はことでとく衝突電離し、そのイオン化率は導入ガス体の性無によって変わるが最大 8 0 5 に達する。

この場合、電子は中空陽極放電管に引きつけられ前失するが、隔イオンは後に残され大きな陽イオンは後に残され大きな陽イオンほとなって中空陽極電位より低い負債の対極(真空チャンパー(7) や基板(6) 等)に向って流出供給される。イオン化された原子は負電位に印加された基板(6) に引かれ電圧条件を任意に調節することでイオンエッチング、イオン注入複合成が可能となり、複の密着性も著しく高いものが得られる。

本発明は種々のガス体においてこのような構成が可能であることを発見し、発明に到ったものでその中空陽極放電における理論的解明に到っていないが中空管形状、放電電離真空度、陽極電位を

in All ( All

要求される特性を持つ僕の合成を可能とならしめた。

一方Arイオン等を中空隔極放電電より供給し

## **转開昭61-143579 (4)**

基板(6)へ照射するととにより、基根表面が不活性 イオンの簡単でクリーニングされ合成機の基板へ の困着性向上を計ることもこの中型場低放電管を 用い、ガスの切換え、印加陽極電位の調節のみで 容易に得られる。

また本発明は従来から使用されているイオン鉄の如く復雑課金を用いず出来るだけ簡素化した構造にすることにより異常発生が極めて少なく、かつ中空陽極に衝突するのは電子のみであるため異

介して中空陽極放電管(I) に供給される。一方との中空陽極放電管(I) は絶縁ガイシ切により真空チャンパーあるいはガス供給機構等とは電気的絶縁状態を保ちながら電源トランス(2) の陽極電位側に接続する。

真空チャンパー(7) は真空排気孔00より外部の真空排気装置に接続され真空状態に保たれ通常アース電位にある。この場合真空度は通常数+Torr~10<sup>-3</sup> Torr 程度を用いる。このような装置構成の中空陽極放電管に射起ガス体を導入し隔極電位を印加することにより前述の通り電子と導入ガス体の著しい衝突電離を可能にし、発生したイオンを真空チャンパー(7) 内の特に図中電源トランス(4) の負電位を印加した基板台(5) あるいは基板(6) に無射供給される。尚電源トランス(4) と真空チャンパー

ユロ・イー・・・ ごを受け、導入できから18。 である場合は基板(6) 上に81個が形成され、場合に よつては基板(6) 中に81イオンが打ち込まれる。ま 常界風や中空陽低管の消耗が極めて少なく使用が 命が著しく長く、中空管材質の溶融蒸発による質 材質への汚染に関する間堰が全く発生しないイオ ン供給表電および方法の提供を可能にした。 (具体的実施塑練)

本界明の具体的実施理様を飛付図面に基づいて 説明するが本発明方法は、とれらのみに限定され るものでない。なお、図中同一符号は同一部材ス は均等部材を示す。

第1図は例えば、Ar, Ne 等の不活性ガス 81日。, Tic 2。等金属結合ガスあるいは Ti ( i ( CB a ) a )。等の有限金属化合物ガス等のうち 1 種類の導入ガス体を用い目的とするイオンの形成、原射を可能ならしめ、不活性ガスイオンによるイオンクリーニング、イオンエッチングあるいは金属薄質の作成化合物薄質の合成を計ることを目的として中空陽極放電管(1) は Ta . No . 同 あるいはステンレス等導電性中空管で形成し、前配導入ガス体はガス供給源的から促量計( g) 、ガス促量調節パルブ04 を

た導入ガスが T1  $\{N(CH_3)_2\}_0$  等の化合物であれば T1(CM) 等の化合物質が基板(6)上合成される。

とのように目的に応じた導入ガス体を用い、陽極電位を調整することによりイオンエッチング、 イオン注入、複合成を行ない得るイオン供給装置 シよび方法が可能になった。

通常直旋電界により導入ガス体が放電し、化合物等の分解、励起イオン化が可能な領域は削速の如く数+ Torr から 1 0<sup>-3</sup> Torr 程度である。しかしながら真空チャンパー(7)の内壁扱着ガスによる基板(6)への汚臭防止あるいはイオンの飛散距離(mean free path ) の増大等を計って処理条件の改善が望まれる場合、真空チャンパー(7)中の真空度を10<sup>-4</sup> Torr とする必要が生ずる場合がある。かかる場合は 2 図に示す如く中空管(1)の先端を収

・ Form 程度で安定性電を存続させたい場合制工会 の如く開先進形状化し中型増(I)の内部と真型チャ シバー(7)の間にできるだけ圧力差を生ぜしめない

## **特開昭61-143579(6)**

構造にすることにより放電の安定化を計るもので もる。

更に第1回において通常放電は中空降極放電管 (1)とそれより負の電位にある着板(6)の間で安定に 持続されるが、中空陽極放電管に印加される正の 電位が数 RV ~数 1 0 RV の場合、中空陽極放電管 (1)と真空チャンパー(7)との間で断続的具常放電を 発生する場合がある。特に中空陽極放電管電位を 高めた状態にて長時間放電させたい場合、第4回 の如く、中空管(1)の表面に A んょう。の 絶縁物質(9)を お射等によりコーティングして使用し、異常放電 発生を防止する必要がある。コーディングする絶 最物質例えば A Li Os の厚みは A Li Os の気孔本組成 等に基づく絶縁度により大きく変位するが絶縁度 が大ならば、通常50/22から3 24で十分可能であ り、それ以上厚みが増すと放電前後の温度差によ るクラック発生が大きくなり、中空管から制度、 難脱するととが多くなる。

第3図は二つ以上の異種ガス体を同時に用い、 複数のイオンを同時に供給する具体的方法をよび

べて前述の範囲内で可能であった。

#### (実施例1)

第1図に示す装置を用い導入ガスを Ti [N(CH<sub>2</sub>)<sub>2</sub>]。 としTiCN製合成を下配の条件で行なった。

中空陽極電圧

真空チャンパー圧力

IXIOTTOTT

中空隔極放電管形状

# 2 5 ma × L 1 0 0 ma

中空陽極放電管電流

4.5 A~ 4.2 A

基板電圧

- 5 0 0 V

基板ヒーチー

207100A~0VOA(8U8パンド

ヒーター)

基板推定温度

\* \* \*

300~400C

板 材 質

H88チップ(8単0単432類似型 )

得られた複組成は TiC に近い銀灰色の TiC N 襲 で HV2000~2200、 X 韓回折の結果 TiC<sub>07</sub> M<sub>03</sub> と判

ほし - 45<sup>3でH</sup>0143~235 / と連続切削試験にて 評価したところ無処理品の切削寿命に対し的 5 倍 の身命向上が確認された。

装置構成を示すものである。中空隔極放電管(1 ~1)、(1~2)は各々電源トランス (2~1)、 ( 2~2)の降極側に接続し、各々の中空降板放 電管はガス供給原からガス調節パルプ(14~1)、 (14~2)を介してガス体を供給する。電気的絶縁 機能、放電中の真空度、放電を可能にする中空管 形状、印加する電極電位はすべて前述の範囲にあ る。このように複数の中空降極放電管により複数 のガス体の化学結合のしかたに応じた陽極電圧印 加により目的に応じたガスイオンの供給が可能と なり化学量論的に正規な際、あるいは一層好まし い特性を持つ化合物関あるいは合金膜の形成を可 能ならしめた。

さらに無き図、第2回の如く1本の中空陽塩法 運賃内に二重、三重あるいは二本、三本の中空間 極管を電気的絶験を保ちつつ配置することで特に 導入ガス体イオンの混合が困難を場合でも化合物 薄膜を任意の組成化で合成することができる方法 シよび装置構成を示すものである。 この場合の印 加陽極電位、中空管形状、放電中の真空度等もす

#### (実施例2)

第5図化示す英雄を用い、導入ガスをTiC4eと し反応ガスとしてMaを用い、中空陽極放電管1~ 1、1~2を用いて『iff 製の合成を下記の条件で 行なった。

中空陽極放電管

1~1

中空陽極電圧

+1300V +1500V

1 ~ 2

中空陽艦形状

#20mx 2100mm #25mx 2100

導入ガス

TICL + H,

中空降極放電々流

25A~28A 3.8 A

真空チャンパー圧力

1×10<sup>-2</sup>Torr

**基板電圧** 

- 8 0 0 V

基植ヒーター

20 V100 ~ 10 V55A (8U8 ペン

ドヒーター)

推定基板基度

400 ~ 500C

中的33多のDと含有度筋もり、 HSS テノブに処理 し S 4 5 C ( N 1 1 8 0 ~ 2 0 0 ) を連続切削試験にて評価 した所無処理品の切削寿命に比べ釣4倍の寿命向

## **特開昭61-143579(6)**

上が確認され、裏の密着性も良好で制御はなく、 中空障循放電によるイオン供給効果の大なること を通常のプラズマ CVD と比較して確認した。 (発明の効果)

本発明に基づく中空降極放電を用いたプラズマ イオン供給装置を使用することにより次のような 効果を発揮する。

- (1) イオン化率が高く、イオン密度の著しく大き い高反応性プラズマイオンの供給が可能。
- 何 こつ以上の異種ガスを使用する場合、それぞ れのガスの分解、励起イオン化に長するエネル ギーに応じ、中空管形状、導入ガス量、印加陽 極電圧等を開節するととにより、最も高いイオ ン化状態でコントロールし、供給することがで きる。・
- 台 何の効果により生成される裏組成を最も望ま しい化合物形態に調整できる。
- 日 為陰値PI3イオン銃等にみられる熱フィラ メント元素の真空蒸発による裏汚象が防止でき、 大イオン電流が得やすく、構造簡便で異常発生

5 … 基 板 台 6 ... 🛎

7…放電室(真空チャンパー)

8 … 基板ヒータ 10 … 真空排気孔

11,12,13 … 絶縁ガイシ

14 … ガス調節パルプ (14-1,14-2,14-3 6 均等 )

代理人 并度士

の頻度が零かもしくはほとんどなくなる。 树 中空隔極放電管は質量の小さな電子循準を受 けるのみで、損傷がたく、寿命が著しく長い。 N ガス状物質として供給できるものであればい かなる元素もイオン化可能で、高いイオン宝度

(ト) 中空陽極放電管IC Be Ne Ar 等の不活性ガスを 導入し、イオン化して基模へ限射することで基 板表面のイオンエッチング、イオンクリーニン グが可能となり、かつ反応ガス体を切換えるだ けで、連続して化合物需要の合成が可能となり その裏の基根との簡着性も著しく強固なものに てきる.

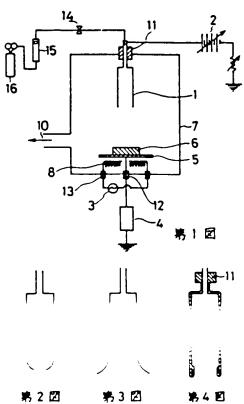
#### 西面の簡単な説明

のイオン供給が可能。

第1回は本発明によるプラズマイオン供給方法 の装置構成を示す略図、第2図、第3図、第4図 は中空管の構成の彩施例、第5回、第6回、第7 図は本発明の他の装置構成例を示す。

1 … 中空管(1-1,1-2,1-3 も均等)

2,4…電源トランス(2-1,2-2,2-3 6 均等)



# 特開昭61-143579 (ア)

